

# Hydrogen Storage with Aluminum Formate, ALF: Experimental, Computational, and Technoeconomic Studies

Hayden A. Evans,\* Taner Yildirim,\* Peng Peng, Yongqiang Cheng, Zeyu Deng, Qiang Zhang, Dinesh Mullangi, Dan Zhao, Pieremanuele Canepa, Hanna M. Breunig, Anthony K. Cheetham, and Craig M. Brown\*



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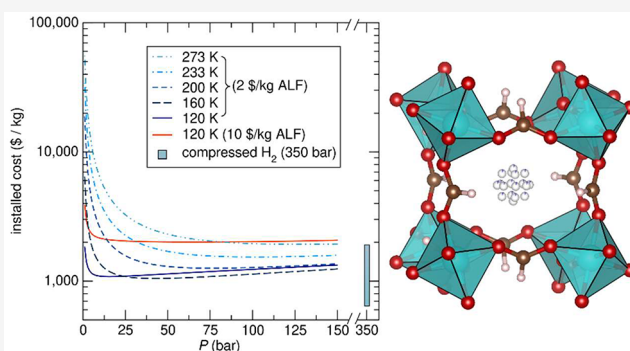


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Supporting Information

**ABSTRACT:** Long-duration storage of hydrogen is necessary for coupling renewable H<sub>2</sub> with stationary fuel cell power applications. In this work, aluminum formate (ALF), which adopts the ReO<sub>3</sub>-type structure, is shown to have remarkable H<sub>2</sub> storage performance at non-cryogenic (>120 K) temperatures and low pressures. The most promising performance of ALF is found between 120 K and 160 K and at 10 bar to 20 bar. The study illustrates H<sub>2</sub> adsorption performance of ALF over the 77 K to 296 K temperature range using gas isotherms, in situ neutron powder diffraction, and DFT calculations, as well as technoeconomic analysis (TEA), illustrating ALF's competitive performance for long-duration storage versus compressed hydrogen and leading metal–organic frameworks. In the TEA, it is shown that ALF's storage capacity, when combined with a temperature/pressure swing process, has advantages versus compressed H<sub>2</sub> at a fraction of the pressure (15 bar versus 350 bar). Given ALF's performance in the 10 bar to 20 bar regime under moderate cooling, it is particularly promising for use in safe storage systems serving fuel cells.



## INTRODUCTION

Stationary hydrogen-powered fuel cells are emerging as a solution for delivering clean and flexible power.<sup>1–3</sup> Renewable-energy-powered electrolysis can generate hydrogen but may require multiple days' worth of hydrogen storage to smooth renewable-energy variability. Storage is also needed in cases where hydrogen is used as a backup power system, with a necessary target storage duration of 96 h to meet the requirements set by the United States National Fire Protection Association. This presents a challenge, as compressed gas or cryogenic hydrogen storage is operationally expensive and inefficient at large scales for these storage durations, and salt caverns proposed for storage are not widely available and require pipelines to make them suitable for significantly larger applications. As such, much work has been conducted to identify material-based solutions for hydrogen storage that operate at lower pressures and warmer temperatures.<sup>4</sup>

A recent analysis by some of the authors of stationary hydrogen storage for long-duration energy supply suggests there is potential for porous metal–organic frameworks (MOFs) to perform well in such applications.<sup>5</sup> These materials can adsorb H<sub>2</sub> within their porous structures and via gas–framework interactions, facilitating high hydrogen storage capacities. However, a MOF's peak adsorption under equilibrium conditions is only one indicator of promise, and

a MOF must be holistically evaluated across other key factors, such as the constraints resulting from integration with electrolyzer and fuel cell systems. Fuel cells require high-purity hydrogen at fast delivery rates and modest pressures, which MOFs are uniquely capable of achieving. Additionally, previous studies have shown that green H<sub>2</sub> generated by on-site electrolyzers tends to be warm ( $\approx 320$  K or above).<sup>6</sup> Storing this warm H<sub>2</sub> under cryogenic temperatures (i.e., 77 K) could lead to high refrigeration costs. For example, for cooling processes below 248 K versus 83 K, the refrigeration cost for 1 MW of cooling load increases from 18.5 \$/GJ to 360 \$/GJ (2017 values), respectively.<sup>7</sup>

Until recently, conventional MOFs for hydrogen storage required low temperatures to achieve high hydrogen uptake.<sup>8,9</sup> Most reported MOFs [e.g., Zn<sub>4</sub>O(BDC)<sub>3</sub> (MOF-5, BDC<sup>2-</sup> = 1,4-benzenedicarboxylate), Cu<sub>3</sub>(BTC)<sub>2</sub> (HKUST-1, BTC<sup>3-</sup> = 1,3,5-benzenetricarboxylate), and CdIF-13 (sod-Cd-(benzimidazolite)<sub>2</sub>)]<sup>10</sup> show maximum hydrogen uptake

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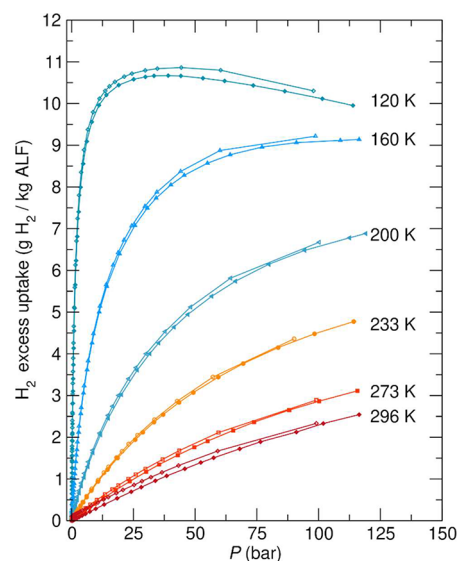
under cryogenic temperature and high-pressure conditions, whereas some emerging MOFs, such as  $\text{Ni}_2(m\text{-dobdc})$  and  $\text{V-btdd}$  ( $m\text{-dobdc}^{4-} = 4,6\text{-dioxido-1,3-benzenedicarboxylate}$ ;  $\text{H}_2\text{btdd} = \text{bis}(1H\text{-}1,2,3\text{-triazolo}[4,5\text{-}b],[4',5'\text{-}i])\text{dibenzo}[1,4]\text{-dioxin}$ ), exhibit record deliverable  $\text{H}_2$  at near-ambient temperatures and high-pressure conditions (i.e., above 100 bar).<sup>11,12</sup> Initial findings suggested that  $\text{Ni}_2(m\text{-dobdc})$  could achieve a lower leveled cost of storage ( $\$/\text{kWh}$ ) relative to cryogenic storage, but not compared to compressed gas storage at 350 bar without  $\text{Ni}_2(m\text{-dobdc})$  being made cheaply and able to retain relatively high hydrogen uptake (i.e., below 10  $\$/\text{kg}$  and above 15  $\text{g}/\text{kg}$  excess uptake).<sup>5</sup> It was also found that slower charging of the storage tank greatly reduced the cost of the associated compression and refrigeration units, further improving the promise of sorbent-based systems.

Recently, work published by researchers here has illustrated the impressive adsorptive properties of one of the simplest and lowest-cost MOF materials, aluminum formate,  $\text{Al}(\text{HCOO})_3$  (ALF). ALF adopts an  $\text{ReO}_3$ -type structure<sup>13</sup> and has been shown to adsorb  $\text{CO}_2$  from dried  $\text{CO}_2$ -rich flue gas conditions with high  $\text{CO}_2/\text{N}_2$  selectivity,<sup>14</sup> to selectively adsorb  $\text{CO}_2$  from any hydrocarbon mixture, including acetylene,<sup>15</sup> and to provide impressive selective  $\text{O}_2$  adsorption characteristics from  $\text{O}_2/\text{N}_2$  mixtures above cryogenic temperatures.<sup>16</sup> Furthermore, ALF has very practical attributes sought for industrially utilized materials, such as withstanding pelletization, being air-stable, and being derived from cheap commodity chemicals.<sup>14</sup> Given the remarkable performance of ALF in these important areas as well as its alluring scalability attributes, we extended our focus to examine whether ALF could be utilized for stationary hydrogen-powered fuel cell applications.

Herein, we demonstrate that ALF displays remarkable  $\text{H}_2$  storage performance above cryogenic temperatures ( $>120\text{ K}$ ), with the most promising performance between 120 K and 160 K. We discuss the  $\text{H}_2$  adsorption performance of ALF over the temperature range from 77 K to 296 K via gas isotherms, the crystal structure of ALF as it adsorbs  $\text{D}_2$  gas, as resolved from in situ neutron powder diffraction, DFT calculations that support the observed performance, and technoeconomic analysis (TEA) illustrating ALF's price-competitive performance versus leading MOFs and compressed hydrogen for long-term storage. For the TEA, we show how the storage capacity of ALF, when combined with a temperature/pressure swing process, gives it clear advantages versus compressed  $\text{H}_2$  at a fraction of the pressure.

## RESULTS AND DISCUSSION

**Gas Isotherm Measurements.** Figure 1 displays the excess gas adsorption/desorption isotherm measurements of ALF at various temperatures plotted as a function of grams of  $\text{H}_2$  adsorbed versus kilograms of ALF. The Supporting Information contains the same data plotted with other metrics, as well as the total adsorption plots, for comparison (Figures S1–S5). As can be seen from Figure 1, ALF shows excess adsorption of  $\text{H}_2$  gas of  $\approx 11\text{ g}$  of  $\text{H}_2$  per kg of ALF near 120 K and  $\approx 25\text{ bar}$  of pressure. As the temperature is increased, the maximum adsorption decreases, as is expected from thermodynamics. Each of the isotherms can be described as Type I isotherms, and from nonlinear Langmuir fits of the excess isotherms (Figure S6), the experimental heat of adsorption for the  $\text{H}_2$  adsorption is 8.67  $\text{kJ}/\text{mol}$  when treated with a single-site Langmuir model.<sup>17</sup> Alternative treatments

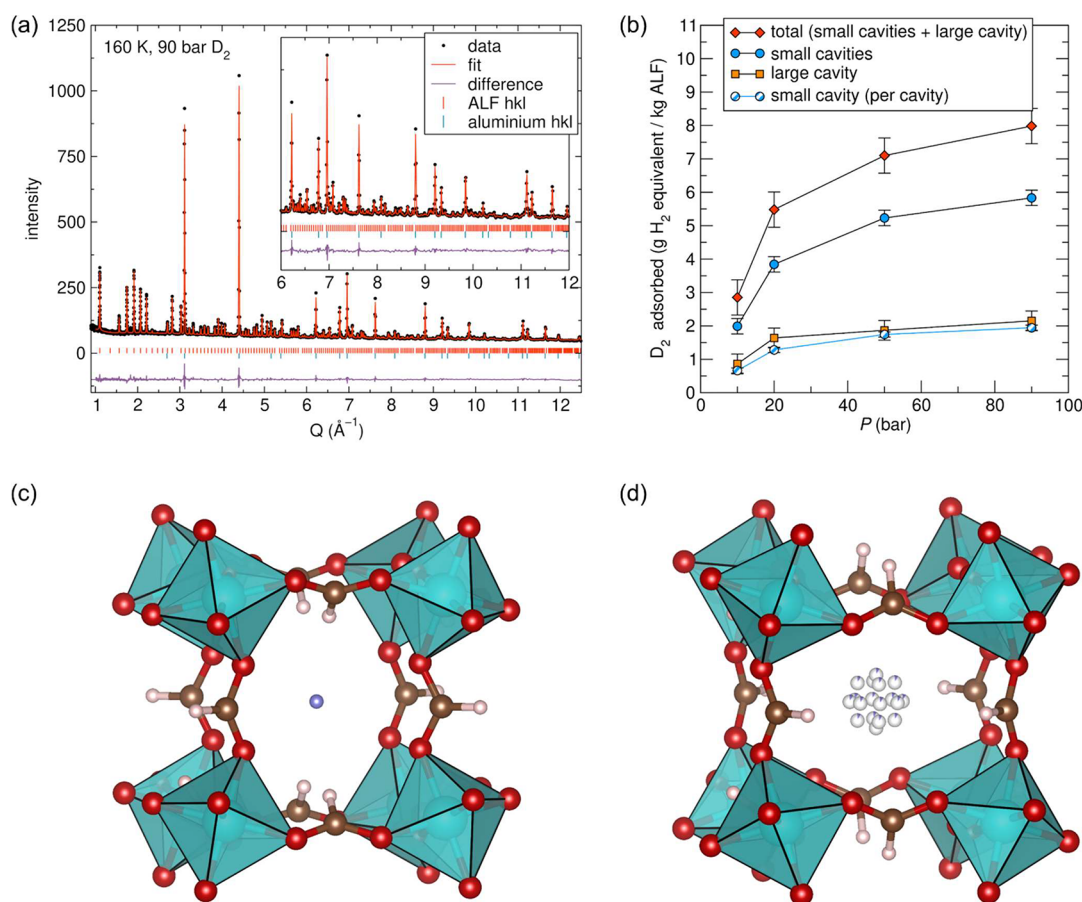


**Figure 1.** Excess  $\text{H}_2$  gas adsorption/desorption isotherm measurements on ALF between 120 K and 296 K. Closed symbols = adsorption, open symbols = desorption. The same data plotted on the y-axis with other metrics are provided in the Supporting Information, alongside total adsorption plots and nonlinear Langmuir fits and data (Figures S1–S11, Tables S1–S4).

using a dual-site Langmuir model with lower and upper bound pore volume considerations can be found in the Supporting Information. The dual-site treatments provide similar heat of adsorption values between  $\approx 8.5\text{ kJ}/\text{mol}$  and  $\approx 9\text{ kJ}/\text{mol}$  as a function of loading. Given the dense, ultramicroporous nature of ALF (a material with pore sizes less than 10 Å; see previous work's supplementary materials for pore diagram)<sup>14</sup> when compared to many large-pore MOFs,<sup>9,12</sup> the adsorption values at increased pressures trend closer to values for compressed hydrogen. Figure S7 illustrates this point by showing the observed volumetric  $\text{H}_2$  storage densities for ALF versus theoretical compressed  $\text{H}_2$  volumetric densities (NIST Web-Book)<sup>18</sup> of a given pressure and temperature swing process ending at 5 bar and 296 K. As such, the large initial  $\text{H}_2$  adsorption at temperatures between 120 K and 200 K and pressures beneath 50 bar offers promising performance for  $\text{H}_2$  storage using ALF.

As temperature is decreased below 120 K (Figures S1–S5), the inherent kinetic effects of ALF grow more pronounced, manifesting as hysteresis between adsorption and desorption curves. We have observed this phenomenon for both  $\text{CO}_2$  and  $\text{O}_2$  adsorption with ALF,<sup>14,16</sup> albeit at different temperatures, given the distinct interactions each gas has with ALF. This kinetic behavior, though curious, is not uncommon for microporous systems and has been observed in such systems as zeolite type A<sup>19</sup> and a non- $\text{ReO}_3$ -type  $\text{Mn}(\text{II})$ -formate.<sup>20</sup> Both materials, much like ALF, display complex sorbate–framework interactions that impact adsorption kinetics. In the case of the  $\text{Mn}(\text{II})$ -formate material, the authors postulated that the material has “dynamic opening of the pore aperture and/or sufficient kinetic energy of the adsorbates to overcome a diffusion barrier above a critical temperature.”<sup>20</sup> We believe that there is a similar effect in ALF and that there is likely a “critical gating temperature” which is dependent on the nature of each specific gas adsorbed into ALF.

**In Situ  $\text{D}_2$  Gas Dosing Powder Neutron Diffraction Studies.** In situ  $\text{D}_2$ -dosed neutron powder diffraction



**Figure 2.** In situ neutron diffraction results on ALF at 160 K under D<sub>2</sub> pressure [ORNL, POWGEN]. (a) Representative Rietveld refinement of ALF under 90 bar of D<sub>2</sub>.  $R_{wp} = 3.92\%$ ,  $R_p = 3.37\%$ . Space group:  $Im\bar{3}$  (No. 204). Lattice parameters,  $a = b = c = 11.3669(1)$  Å. Aluminum  $hkl$ 's refer to solid Al high-pressure sample used for experiment, not Al metal within the sample. Refinement results can be found in the [Supporting Information](#), Figures S12–S16, Tables S5–S9. (b) Refined values of D<sub>2</sub> occupancy found within ALF from the 160 K data sets for each cavity, converted into equivalent grams of H<sub>2</sub> per kilogram of ALF (using a molecular mass of 2 g/mol instead of 4 g/mol (D<sub>2</sub>)) for direct comparison with [Figure 1](#). These results are also shown in the [Supporting Information](#) (Figure S17) as a function of mmol D<sub>2</sub>/g ALF and g D<sub>2</sub>/kg ALF. Error bars and values denote  $1\sigma$ . (c) Small cavity (SC) of ALF with D<sub>2</sub> super-atom at the center of the cavity. (d) Large cavity (LC) of ALF with D<sub>2</sub> super-atom disordered over the surface of a sphere (radius = 0.677 Å).

experiments on ALF were conducted at the POWGEN instrument at Oak Ridge National Laboratory. Experiments were conducted at 160 K under multiple pressures of D<sub>2</sub> gas (0 bar, 10 bar, 20 bar, 50 bar, and 90 bar) to resolve how the structure of ALF filled and/or changed with D<sub>2</sub> gas. The 160 K temperature was chosen for the experiments as adsorption was known to be both fast and in high enough quantities to ensure that reliable positions of the D<sub>2</sub> molecules could be located within the allotted experimental time frame. Furthermore, given the fast onset of H<sub>2</sub> adsorption at 120 K, conducting the experiments at 160 K also allowed incremental observation of the adsorption of D<sub>2</sub> into the structure of the ALF to be done more precisely.

As discussed in previous work, ALF adopts an ReO<sub>3</sub>-type structure.<sup>13</sup> It is akin to the perovskite structure, only instead of an A-site cation there is a vacancy (void space). The structure of ALF is found in the  $Im\bar{3}$  space group and, as a result, has two crystallographically distinct cavities, denoted as the small cavity (SC) and large cavity (LC), which differ by how the hydrogens of the formates point toward or away from the center of each cavity, respectively. The pore volumes for the SC and LC at 300 K are 43(3) Å<sup>3</sup> and 79(9) Å<sup>3</sup>, respectively.<sup>14</sup> For CO<sub>2</sub> adsorption, the SC favors CO<sub>2</sub>

adsorption relative to the LC because the hydrogen bonding from the formate hydrogens engages in a “hand-in-glove” interaction with CO<sub>2</sub>. This contrasts what was observed for O<sub>2</sub> adsorption in ALF, where hydrogen bonding in the SC is found to be less significant, with a slight preference for the LC.<sup>16</sup> This slight preference for the LC is observed here for D<sub>2</sub> adsorption as well, as we will now discuss.

[Figure 2](#) shows select results from the in situ gas-dosed neutron powder diffraction experiments, including visualization of the D<sub>2</sub> positioning within the crystal structure of ALF obtained from Rietveld-derived chemical models. [Figure 2a](#) shows a representative Rietveld refinement fit of the data acquired for the highest dosed D<sub>2</sub> condition, 90 bar. This data set was used to confidently resolve the positions of the D<sub>2</sub> gas molecules adsorbed within ALF, which were then used for the lower pressure data sets. The [Supporting Information](#) shows the refinement fits obtained for the other pressures tested (0 bar, 10 bar, 20 bar, and 50 bar). Specific to the refinements, the gas molecules were modeled as “super-atoms”, given that D<sub>2</sub> is a quantum object and the molecular dumbbell is orientationally averaged to produce a more spherical scattering center, as is typically observed in the literature.<sup>12,21–24</sup> Practically, this means that an appropriate Rietveld refinement will use a single

D atom, instead of a D<sub>2</sub> molecule, to describe a D<sub>2</sub> molecular position. In the refinements, each D super-atom was allowed a maximum occupancy of 2 to account for the modeling of a D<sub>2</sub> molecule.

Figure 2b shows the refined amounts of D<sub>2</sub> adsorbed in ALF as derived from the Rietveld refinements over the range of pressures studied. The amounts graphed are the total amount adsorbed at each pressure, as well as the amount for each cavity. The occupancies in Figure 2b have been converted to grams of H<sub>2</sub> per kilogram of ALF, for direct comparison with the isotherm data in Figure 1. The metrics in mmol of D<sub>2</sub> per g of ALF, and g of D<sub>2</sub> per kg of ALF, are also found in the Supporting Information (Figure S17). Tables S5–S9 in the Supporting Information show the crystallographic occupancies from the refinements prior to conversion. As can be appreciated, the power of the in situ gas dosing neutron diffraction experiments is that the Rietveld refinements with such data provide real-space context as to how gases interact with an adsorbent.<sup>25</sup> In this instance, we found that, at all D<sub>2</sub> pressures tested, and given that ALF has two distinct cavities, the SC and LC, both cavities adsorbed D<sub>2</sub> gas in nearly equal amounts after equilibration when normalized for multiplicity. This is shown in Figure 2b when comparing the D<sub>2</sub> occupancy of the LC versus the D<sub>2</sub> occupancy found in just one SC (there are 3 times as many SCs versus LCs within ALF, given the *Im* $\bar{3}$  symmetry).

Though D<sub>2</sub> is adsorbed into each of the cavities in nearly equal proportions, how the D<sub>2</sub> molecules fill within the two cavities is distinct. Figure 2c,d illustrates how the D super-atoms are found within the SCs and LCs, respectively, as resolved from the Rietveld refinement with the data at 160 K and 90 bar D<sub>2</sub> pressure. The SC D super-atom was found to be best modeled with one position at the special position [0, 1/2, 0], which is the center of the SC. Attempts were made to move the super-atom off this special position within the SC, which in principle could describe any preferential positioning within the cavity. However, no position away from the [0, 1/2, 0] position was found to statistically improve the fit or provide any other convincing indications of localization. Instead, the most stable and statistically consistent result was modeled with a super-atom at the center of the cavity with a large isotropic Debye–Waller factor,  $B_{\text{eq}}$  (refined and stable  $B_{\text{eq}}$  value of  $\approx 14 \text{ \AA}^2$ ). This result implies that the D<sub>2</sub> inside of the SC is, on average, localized at the center of the cavity, albeit likely somewhat dynamic under these conditions.

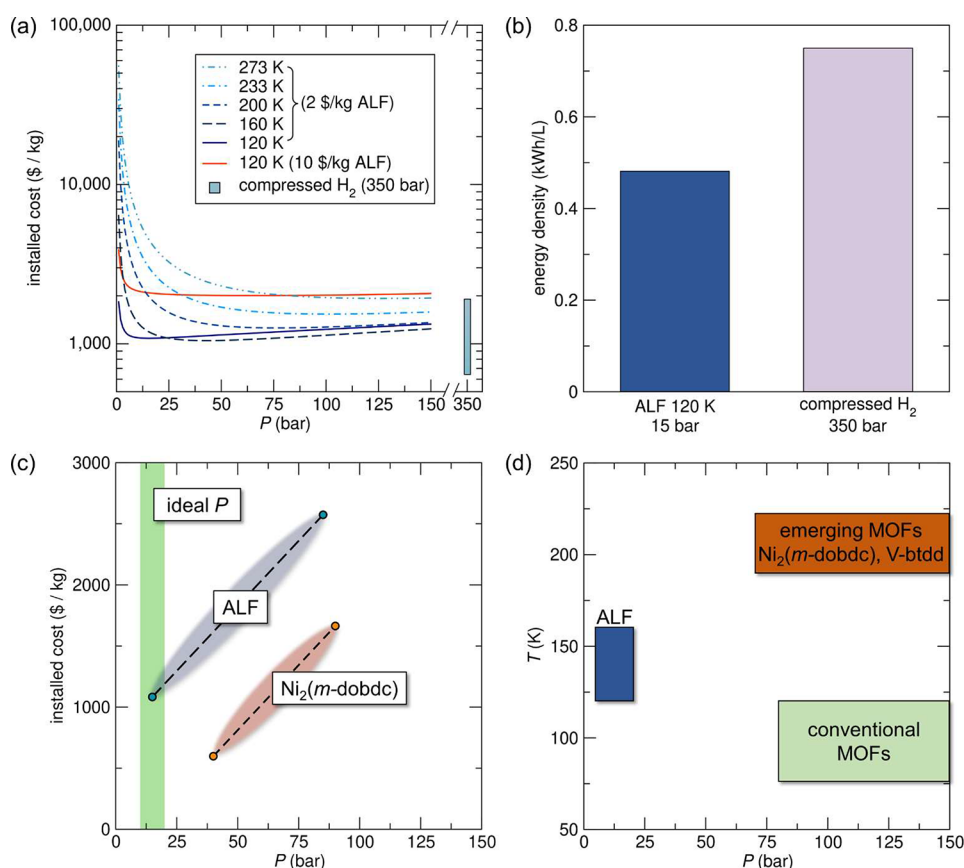
This result contrasts with what was found to be the case for the LC, where if the D super-atoms were modeled at the center of the LC, they had a refined  $B_{\text{eq}}$  of  $\approx 14.2 \text{ \AA}^2$ , similar to that of the SC D super-atom. However, if they were displaced from the special position so as to populate the surface of the sphere inside of the LC, the  $B_{\text{eq}}$  values of the D super-atoms were reduced and stabilized by an order of magnitude to  $\approx 1.7 \text{ \AA}^2$ . This spherical surface modeling is shown in Figure 2d. This indicates that there is preferential adsorption of the D<sub>2</sub> gas toward the surfaces of the LC walls/ligands, as opposed to occupying the center of the cavity. The distinction in the localization of D<sub>2</sub> within the two cavities can be rationalized given that there is likely vibrational movement of the formates/formate hydrogens at these temperatures that would constantly perturb the location of the D<sub>2</sub> molecules when at the center of the SC. Given that the LC has no such formate hydrogens that point inward, the D<sub>2</sub> molecules could be expected to be comparatively undisturbed, as they associate with the formate

ligands' O–C–O backbone through weak electrostatic and other dispersion forces. This model is further supported by a DFT-derived heatmap for H<sub>2</sub> positional energy inside the cavities of ALF. The heatmap suggests the existence of a shallow energy landscape for H<sub>2</sub> toward the walls of the LC, contrasting with a clear localized low-energy landscape for H<sub>2</sub> positioned at the center of the SC (Figure S18). There is also excellent agreement between the total hydrogen capacity of the pores and that expected from the 160 K adsorption isotherm.

Furthermore, in agreement with our diffraction and isotherm results, the DFT-calculated H<sub>2</sub> heats of adsorption for each of the cavities are found to be 11.66 kJ/mol and 12.54 kJ/mol for the SC and LC, respectively (details in Supporting Information). These similarly valued heats of adsorption for the two cavities align well with what was seen from diffraction, which suggests that H<sub>2</sub> fills both cavities with comparable amounts, with a slight preference for the LC. The DFT-calculated heat of adsorption values are also close to the isotherm-derived heat of adsorption of 8.67 kJ/mol (fitting from nonlinear Langmuir fits to the adsorption data 120 K to 297 K, Figure S6). It is understood from the literature that the optimal heat of adsorption for hydrogen storage materials at ambient conditions should be between 15 kJ/mol and 25 kJ/mol.<sup>12</sup>

**Technoeconomic Analysis (TEA) of Stationary Long-Duration H<sub>2</sub> Storage Using ALF.** Materials proposed for on-board H<sub>2</sub> use,<sup>26–29</sup> including V-btdd<sup>12</sup> and Ni<sub>2</sub>(*m*-dobdc),<sup>11</sup> are judged most significantly by their high H<sub>2</sub> storage densities as close to room temperature as possible. This contrasts with the requirements of long-duration H<sub>2</sub> storage materials, where H<sub>2</sub> storage density is not the most important factor, given that space is not limited as it would be in a vehicle. Instead, materials for long-duration H<sub>2</sub> storage are judged by their general performance (adsorption per *T* and *P*), scalability, and cost. ALF distinguishes itself in this regard from most MOF materials proposed for long-duration H<sub>2</sub> storage by being derived from low-cost commodity chemicals and still achieving high H<sub>2</sub> uptakes at low working pressures and non-cryogenic temperatures. We evaluate the impact of these characteristics on the cost for an on-site, large-scale (10 MW), and long-duration (96 h) stationary H<sub>2</sub> storage application to meet backup power needs (8 cycles per year). We note that, while the reported cycle lives for many MOFs are from 1000 cycles to 5000 cycles,<sup>30,31</sup> the effects of replacement and stability should be evaluated for future studies requiring more operation cycles. Low-pressure operation is compelling, as a storage pressure between 10 bar and 25 bar is all that is needed for serving the pressure requirements of stationary fuel cells operating at 2 bar to 10 bar.<sup>32</sup> Beyond economic considerations, operating storage systems at low pressures also greatly reduces the safety concerns and system complexity when dispensing H<sub>2</sub>, providing lower system costs and fostering general public acceptance of the technology.

With regard to material costs, at high manufacturing rates, it has been suggested that emerging MOFs that are manufactured using abundant metals, such as nickel or zinc, can achieve a material cost of 10 \$/kg of MOF.<sup>33</sup> Lowering the MOF manufacture cost to the level of  $\approx 2$  \$/kg, which is expected with ALF given that it is made from the abundant commodity chemical reagents aluminum hydroxide and formic acid (priced at 0.3 \$/kg to 0.5 \$/kg and 0.5 \$/kg to 0.9 \$/kg wholesale costs, respectively, Supporting Information), provides a cost reduction with substantial promise. ALF avoids the use of



**Figure 3.** Technoeconomic analysis (TEA) and system-level performance of ALF vs compressed gas and other MOFs. (a) Modeled installed capital cost for ALF at different temperatures and pressures when the charging rate is half of the discharge rate. The red line shows the installed cost if ALF was priced at 10 \$/kg. Compressed gas installed costs at 350 bar are shown by the light blue bar. (b) Comparison of system-level energy density of ALF with compressed hydrogen storage under 350 bar (293 K), calculated based on the amount of hydrogen stored in a tank and the tank's outer volume. (c) Comparison of ALF with a top-performing contemporary MOF ( $\text{Ni}_2(m\text{-dobdc})$ ) under optimum cost and pressures versus under different manufacturing costs and operating conditions [low-cost value, 2 \$/kg with moderate charging (charge = 0.5 times discharge) and high-cost value, 10 \$/kg with fast charging (charge = 4 times faster than the discharge) for both MOFs]. The green area denotes the ideal delivery pressure range (10 bar to 20 bar) for stationary applications when coupled with fuel cells. Dashed lines between the two data points for ALF and  $\text{Ni}_2(m\text{-dobdc})$  are used for an easier comparison between the ranges. The shaded region behind the line denotes that values between the two ranges can vary. (d) Schematic diagram depicting the optimum range of temperature and pressure conditions for different types of MOFs.

comparatively complex organic reagents such as 2,5-dihydroxyterephthalic acid or metal salts such as nickel nitrate (priced at 2 \$/kg to 20 \$/kg and 3 \$/kg to 15 \$/kg, respectively, Supporting Information). Assuming a conservative material cost of 2 \$/kg and based on the H<sub>2</sub> excess uptake with ALF (Figure 1) and its other fundamental properties (density, specific heat, etc.), we find that a minimum installed cost is achieved at a working pressure near 15 bar (Figure 3a). At this pressure and under moderate cooling (120 K), the modeled ALF (with packing density of 1429 kg/m<sup>3</sup>) achieves approximately two-thirds of the system-level energy density of 350 bar compressed gas storage at ambient conditions (Figure 3b). This represents a  $\approx 95\%$  pressure reduction for comparable performance when using ALF. Furthermore, we again mention that ALF withstands pelletization and ball-milling,<sup>14</sup> making it promising to achieve high packing densities during deployment, which contributes to high system-level energy density.

If such low material costs can be achieved, ALF offers an installed cost that is lower than those of 350 bar compressed gas systems, despite its cooling requirement (Figure 3a). This is true even at a working temperature of 273 K; however, more pressure is required for ALF to achieve costs that are

comparable with those of 350 bar compressed gas systems. A low material cost, such as ALF, would also put the capital cost of a MOF on par with other system components, such as compressors and refrigerators (Supporting Information, Figure S19). We compare ALF to an emerging leader for H<sub>2</sub> storage,  $\text{Ni}_2(m\text{-dobdc})$ , to illustrate each material's optimal operation range based on their cost performance across 120 K to 293 K and 0 bar to 170 bar (Figure 3c). The findings are remarkable, as both ALF and  $\text{Ni}_2(m\text{-dobdc})$  could achieve a lower installed cost than 350 bar compressed gas systems. To our knowledge, this is the first study where sorbent-based hydrogen storage outperforms cryogenic and compressed gas technologies in a hydrogen storage application.

Lastly, the unique adsorption attributes of ALF compared to contemporary MOFs provide new opportunities for future applications for H<sub>2</sub> storage (Figure 3d). ALF's optimum conditions use moderate cooling and low pressures to achieve high storage, potentially making ALF suitable for applications where a precooled hydrogen stream requires storage, as may be the case for the capture of cryogenic boil-off gas.<sup>34</sup>

## CONCLUSION

Herein, we have shown that aluminum formate (ALF), which adopts the  $\text{ReO}_3$ -type structure, adsorbs  $\text{H}_2$  at non-cryogenic temperatures with an experimental heat of adsorption of  $\approx 8.6$  kJ/mol. From the in situ neutron diffraction analysis of  $\text{D}_2$ -dosed ALF, we show how both of ALF's cavities fill at comparable levels. Specifically, the large cavity of ALF has more localized  $\text{D}_2$  molecules near the walls of the framework, while in the small cavity  $\text{D}_2$  molecules are located near the center. The adsorption isotherms show that the optimal performance of ALF is found at relatively low pressures (around 25 bar), where the total uptake is near 12 g of  $\text{H}_2$ /kg of ALF at 120 K. Most importantly, ALF's  $\text{H}_2$  adsorption performance makes it unique compared to other reported MOFs for low-pressure applications at intermediate temperatures.

From TEA, we have shown that ALF is the only MOF to date to achieve cost parity with 350 bar compressed gas storage at a working pressure within the ideal operation range for safe storage systems serving fuel cells. This is achieved at non-cryogenic temperatures, with the best cost performance found between 120 K and 160 K. Given its lower pressure adsorption performance, ALF also shows promise in emerging  $\text{H}_2$  storage/capture areas of interest, such as  $\text{H}_2$  boil-off capture. These results are impressive alone but are further amplified by the practical attributes of ALF for industrially relevant processes. First, ALF is pelletizable, as demonstrated previously,<sup>14</sup> contrasting many large void space MOFs that often amorphize upon pelletization.<sup>35</sup> Second, ALF is chemically robust, withstanding weeks at ambient air conditions without major degradation.<sup>14</sup> Lastly, as ALF is made from cheap and ubiquitous commodity chemicals, it faces fewer challenges in scalability compared to most other MOFs (note our previous demonstration of kilogram-scale synthesis of ALF using laboratory methods<sup>14</sup>). Such characteristics are key for unlocking opportunities for sorbent-based hydrogen storage, as are the proper identification of market applications with sorbent behavior and ideal operating conditions. As cooling adds refrigeration costs, ALF will benefit from applications where low pressure and cool or near-ambient hydrogen are available and storage is required.

## ASSOCIATED CONTENT

### Supporting Information

The Supporting Information is available free of charge at <https://pubs.acs.org/doi/10.1021/jacs.3c08037>.

Experimental details and supporting figures and tables (PDF)

### Accession Codes

CCDC 2264160 contains the supplementary crystallographic data for this paper. These data can be obtained free of charge via [www.ccdc.cam.ac.uk/data\\_request/cif](http://www.ccdc.cam.ac.uk/data_request/cif), or by emailing [data\\_request@ccdc.cam.ac.uk](mailto:data_request@ccdc.cam.ac.uk), or by contacting The Cambridge Crystallographic Data Centre, 12 Union Road, Cambridge CB2 1EZ, UK; fax: +44 1223 336033.

## AUTHOR INFORMATION

### Corresponding Authors

**Hayden A. Evans** – Center for Neutron Research, National Institute of Standards and Technology, Gaithersburg, Maryland 20899, United States; [orcid.org/0000-0002-1331-4274](https://orcid.org/0000-0002-1331-4274); Email: [hayden.evans@nist.gov](mailto:hayden.evans@nist.gov)

**Taner Yildirim** – Center for Neutron Research, National Institute of Standards and Technology, Gaithersburg, Maryland 20899, United States; Email: [taner.yildirim@nist.gov](mailto:taner.yildirim@nist.gov)

**Craig M. Brown** – Center for Neutron Research, National Institute of Standards and Technology, Gaithersburg, Maryland 20899, United States; [orcid.org/0000-0002-9637-9355](https://orcid.org/0000-0002-9637-9355); Email: [craig.brown@nist.gov](mailto:craig.brown@nist.gov)

## Authors

**Peng Peng** – Energy Analysis and Environmental Impacts Division, Lawrence Berkeley National Laboratory, Berkeley, California 94720, United States; [orcid.org/0000-0001-6554-2247](https://orcid.org/0000-0001-6554-2247)

**Yongqiang Cheng** – Neutron Scattering Division, Oak Ridge National Laboratory, Oak Ridge, Tennessee 37830, United States; [orcid.org/0000-0002-3263-4812](https://orcid.org/0000-0002-3263-4812)

**Zeyu Deng** – Department of Materials Science and Engineering, National University of Singapore, 117575, Singapore; [orcid.org/0000-0003-0109-9367](https://orcid.org/0000-0003-0109-9367)

**Qiang Zhang** – Neutron Scattering Division, Oak Ridge National Laboratory, Oak Ridge, Tennessee 37830, United States; [orcid.org/0000-0003-0389-7039](https://orcid.org/0000-0003-0389-7039)

**Dinesh Mullangi** – Department of Materials Science and Engineering, National University of Singapore, 117575, Singapore; [orcid.org/0000-0003-4012-0587](https://orcid.org/0000-0003-4012-0587)

**Dan Zhao** – Department of Chemical and Biomolecular Engineering, National University of Singapore, 117575, Singapore; [orcid.org/0000-0002-4427-2150](https://orcid.org/0000-0002-4427-2150)

**Pieremanuele Canepa** – Department of Materials Science and Engineering, National University of Singapore, 117575, Singapore; [orcid.org/0000-0002-5168-9253](https://orcid.org/0000-0002-5168-9253)

**Hanna M. Breunig** – Energy Analysis and Environmental Impacts Division, Lawrence Berkeley National Laboratory, Berkeley, California 94720, United States; [orcid.org/0000-0002-4727-424X](https://orcid.org/0000-0002-4727-424X)

**Anthony K. Cheetham** – Department of Materials Science and Engineering, National University of Singapore, 117575, Singapore; Materials Research Laboratory, University of California, Santa Barbara, California 93106, United States; [orcid.org/0000-0003-1518-4845](https://orcid.org/0000-0003-1518-4845)

Complete contact information is available at: <https://pubs.acs.org/10.1021/jacs.3c08037>

## Notes

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The authors declare the following competing financial interest(s): A patent has been filed protecting certain information disclosed within this manuscript.

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